# 7.0 A Adjustable Linear Regulator

The CS5207–1 linear regulator provides 7.0 A adjustable voltages with an accuracy of  $\pm 1.5$  %. Two external resistors are used to set the output voltage within a 1.25 V to 13 V range.

The regulator is intended for use as post regulator and microprocessor supply. The fast loop response and low dropout voltage make this regulator ideal for applications where low voltage operation and good transient response are important.

The circuit is designed to operate with dropout voltages as low as  $1.0~\rm V$  depending on the output current. The maximum quiescent current is only  $10~\rm mA$  at full load.

The regulator is fully protected against overload conditions with protection circuitry for Safe Operating Area (SOA), overcurrent and thermal shutdown.

The regulator is available in TO–220 package. A 3.3 V, fixed version is also available. Please consult your local sales representative for more information.

#### **Features**

- Output Current to 7.0 A
- Output Trimmed to ±1.5%
- Dropout Voltage 1.4 V @ 7.0 A
- Fast Transient Response
- Fault Protection Circuitry
  - Thermal Shutdown
  - Overcurrent Protection
  - Safe Area Protection

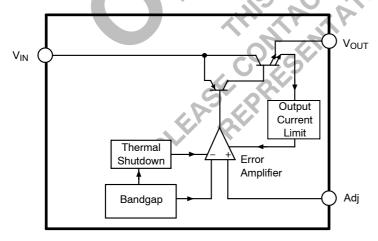


Figure 1. Block Diagram

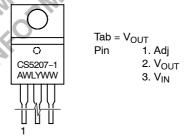


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## PIN CONNECTIONS AND MARKING DIAGRAMS



A = Assembly Location

WL, L = Wafer Lot YY, Y = Year WW, W = Work Week

#### **ORDERING INFORMATION\***†

Device	Package	Shipping		
CS5207-1GT3	TO-220‡	50 Units/Rail		

\*Additional ordering information can be found on page 6 of this data sheet.

†Consult your local sales representative for fixed output voltage versions.

‡TO-220 is 3-pin, straight leaded.

#### CS5207-1

#### **MAXIMUM RATINGS\***

Parameter		Unit
Supply Voltage, V <sub>CC</sub>	17	٧
Operating Temperature Range	-40 to +70	°C
Junction Temperature	150	°C
Storage Temperature Range	-60 to +150	°C
Lead Temperature Soldering: Wave Solder (through hole styles only) Note 1	260 Peak	°C

<sup>1. 10</sup> second maximum.

**ELECTRICAL CHARACTERISTICS** ( $C_{IN}$  = 10  $\mu$ F,  $C_{OUT}$  = 22  $\mu$ F Tantalum,  $V_{IN}$  –  $V_{OUT}$  = 3.0 V,  $V_{IN}$  ≤ 15 V, 0°C[ $\not$ s T<sub>A</sub> ≤ 70°C, T<sub>J</sub> ≤ +150°C, unless otherwise specified, I<sub>full load</sub> = 7.0 A)

Characteristic	Test Conditions	Min	Тур	Max	Unit
Adjustable Output Voltage				0	
Reference Voltage (Notes 2 and 3)	$V_{IN} - V_{OUT} = 1.6 \text{ V}; V_{Adj} = 0 \text{ V}$ 10 mA \leq $I_{OUT} \leq 7.0 \text{ A}$	1.235 (-1.5%)	1.254	1,272 (+1.5%)	V
Line Regulation	$1.6 \text{ V} \le \text{V}_{\text{IN}} - \text{V}_{\text{OUT}} \le 6.0 \text{ V}; \text{I}_{\text{OUT}} = 10 \text{ mA}$	_	0.04	0.20	%
Load Regulation (Notes 2 and 3)	$V_{IN} - V_{OUT} = 1.6 \text{ V}; 10 \text{ mA} \le I_{OUT} \le 7.0 \text{ A}$	/ <del>-</del>	0.13	0.5	%
Dropout Voltage (Note 4)	I <sub>OUT</sub> = 7.0 A	-0	1.4	1.55	V
Current Limit	$V_{IN} - V_{OUT} = 3.0 \text{ V}; T_{J} \ge 25^{\circ}\text{C}$ $V_{IN} - V_{OUT} = 9.0 \text{ V}$	11 <u>-</u> 27	8.5 1.0	- -	A A
Minimum Load Current	V <sub>IN</sub> – V <sub>OUT</sub> = 7.0 V	.0	1.2	6.0	mA
Adjust Pin Current	- 8 4	<u></u>	50	100	μΑ
Adjust Pin Current Change	$1.6 \text{ V} \le \text{V}_{\text{IN}} - \text{V}_{\text{OUT}} \le 4.0 \text{ V}; 10 \text{ mA} \le \text{I}_{\text{OUT}} \le 7.0 \text{ A}$	-	0.2	5.0	μΑ
Thermal Regulation	30 ms Pulse, T <sub>A</sub> = 25°C	-	0.003	-	%W
Ripple Rejection	$f = 120 \text{ Hz}; C_{Adj} = 25 \mu\text{F}; I_{OUT} = 7.0 \text{ A}$	-	80	-	dB
Temperature Stability	0,4-,9,6	_	0.5	-	%
RMS Output Noise	10 Hz ≤ f ≤ 10 kHz; T <sub>A</sub> = 25°C	_	0.003	-	%V <sub>OUT</sub>
Thermal Shutdown	71, 71, 41,	150	180	-	°C
Thermal Shutdown Hysteresis	06.75	-	25	-	°C

<sup>2.</sup> Load regulation and output voltage are measured at a constant junction temperature by low duty cycle pulse testing. Changes in output voltage due to thermal gradients or temperature changes must be taken into account seperately.

### PACKAGE PIN DESCRIPTION

Package Pin Number		
TO-220	Pin Symbol	Function
1	Adj	Adjust pin (low side of the internal reference).
2	V <sub>OUT</sub>	Regulated output voltage (case).
3	V <sub>IN</sub>	Input voltage.

<sup>\*</sup>The maximum package power dissipation must be observed.

Specifications apply for an external Kelvin sense connection at a point on the output pin 1/4" from the bottom of the package.
 Dropout voltage is a measurement of the minimum input/output differential at full load.

#### TYPICAL PERFORMANCE CHARACTERISTICS

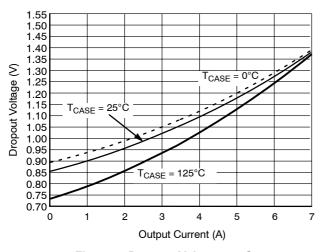


Figure 2. Dropout Voltage vs. Output Current

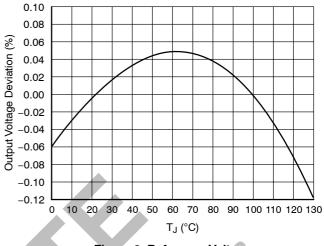


Figure 3. Reference Voltage vs. Temperature

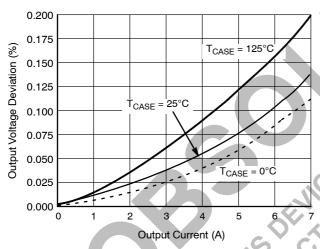


Figure 4. Load Regulation vs. Output Current

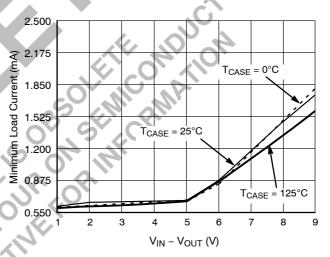


Figure 5. Minimum Load Current

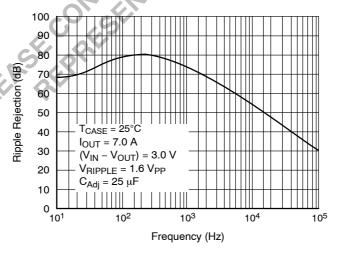


Figure 6. Ripple Rejection vs. Frequency

#### **APPLICATIONS INFORMATION**

The CS5207-1 linear regulator provides adjustable voltages at currents up to 7.0 A. The regulator is protected against short circuit, and includes thermal shutdown and safe area protection (SOA) circuitry. The SOA protection circuitry decreases the maximum available output current as the input-output differential voltage increases.

The CS5207-1 has a composite PNP-NPN output transistor and requires an output capacitor for stability. A detailed procedure for selecting this capacitor is included in the Stability Considerations section.

#### **Adjustable Operation**

The adjustable regulator has an output voltage range of 1.25 V to 13 V. An external resistor divider sets the output voltage as shown in Figure 7. The regulator maintains a fixed 1.25V (typical) reference between the output pin and the adjust pin.

A resistor divider network R1 and R2 causes a fixed current to flow to ground. This current creates a voltage across R2 that adds to the 1.25 V across R1 and sets the overall output voltage. The adjust pin current (typically 50  $\mu A$ ) also flows through R2 and adds a small error that should be taken into account if precise adjustment of  $V_{OUT}$  is necessary.

The output voltage is set according to the formula:

$$V_{OUT} = V_{REF} \times \left(\frac{R1 + R2}{R1}\right) + I_{Adj} \times R2$$

The term  $I_{Adj} \times R2$  represents the error added by the adjust pin current.

R1 is chosen so that the minimum load current is at least 10 mA. R1 and R2 should be the same type, e.g. metal film for best tracking over temperature. The adjust pin is bypassed to improve the transient response and ripple rejection of the regulator.

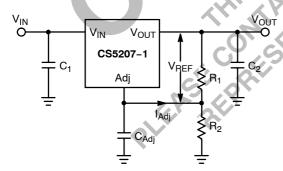


Figure 7. Resistor Divider Scheme for the Adjustable Version

#### **Stability Considerations**

The output or compensation capacitor helps determine three main characteristics of a linear regulator: start-up delay, load transient response, and loop stability. The capacitor value and type is based on cost, availability, size and temperature constraints. A tantalum or aluminum electrolytic capacitor is best, since a film or ceramic capacitor with almost zero ESR can cause instability. The aluminum electrolytic capacitor is the least expensive solution. However, when the circuit operates at low temperatures, both the value and ESR of the capacitor will vary considerably. The capacitor manufacturer's data sheet provides this information.

A 22  $\mu F$  tantalum capacitor will work for most applications, but with high current regulators such as the CS5207–1 the transient response and stability improve with higher values of capacitor. The majority of applications for this regulator involve large changes in load current so the output capacitor must supply the instantaneous load current. The ESR of the output capacitor causes an immediate drop in output voltage given by:

$$\Delta V = \Delta I \times ESR$$

For microprocessor applications it is customary to use an output capacitor network consisting of several tantalum and ceramic capacitors in parallel. This reduces the overall ESR and reduces the instantaneous output voltage drop under transient load conditions. The output capacitor network should be as close to the load as possible for the best results.

#### **Protection Diodes**

When large external capacitors are used with a linear regulator it is sometimes necessary to add protection diodes. If the input voltage of the regulator gets shorted, the output capacitor will discharge into the output of the regulator. The discharge current depends on the value of the capacitor, the output voltage and the rate at which  $V_{\rm IN}$  drops. In the CS5207–1 linear regulator, the discharge path is through a large junction and protection diodes are not usually needed. If the regulator is used with large values of output capacitance and the input voltage is instantaneously shorted to ground, damage can occur. In this case, a diode connected as shown in Figure 8 is recommended.

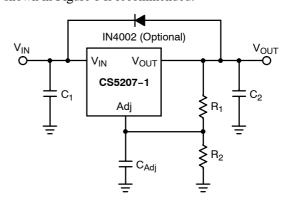


Figure 8. Protection Diode Scheme for Adjustable Output Regulator

#### **Output Voltage Sensing**

Since the CS5207-1 is a three terminal regulator, it is not possible to provide true remote load sensing. Load regulation is limited by the resistance of the conductors connecting the regulator to the load.

Best load regulation occurs when R1 is connected directly to the output pin of the regulator as shown in Figure 9. If R1 is connected to the load,  $R_C$  is multiplied by the divider ratio and the effective resistance between the regulator and the load becomes.

$$R_C \times \left(\frac{R1 + R2}{R1}\right)$$

where  $R_C$  = conductor parasitic resistance.

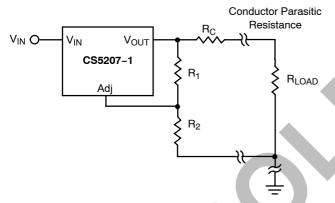


Figure 9. Grounding Scheme for Adjustable Output Regulator to Minimize Parasitic Resistance Effects

### Calculating Power Dissipation and Heat Sink Requirements

The CS5207-1 linear regulator includes thermal shutdown and safe operating area circuitry to protect the device. High power regulators such as these usually operate at high junction temperatures so it is important to calculate the power dissipation and junction temperatures accurately to ensure that an adequate heat sink is used.

The case is connected to  $V_{OUT}$  on the CS5207–1, electrical isolation may be required for some applications. Thermal compound should always be used with high current regulators such as these.

The thermal characteristics of an IC depend on the following four factors:

- 1. Maximum Ambient Temperature T<sub>A</sub> (°C)
- 2. Power dissipation P<sub>D</sub> (Watts)
- 3. Maximum junction temperature T<sub>J</sub> (°C)
- Thermal resistance junction to ambient R<sub>ΘJA</sub> (°C/W)

These four are related by the equation

$$T_{J} = T_{A} + P_{D} \times R_{\Theta JA} \tag{1}$$

The maximum ambient temperature and the power dissipation are determined by the design while the maximum junction temperature and the thermal resistance depend on the manufacturer and the package type.

The maximum power dissipation for a regulator is:

$$P_{D(max)} = \{V_{IN(max)} - V_{OUT(min)}\}I_{OUT(max)} + V_{IN(max)}I_{Q}$$
(2)

where:

V<sub>IN(max)</sub> is the maximum input voltage,

V<sub>OUT(min)</sub> is the minimum output voltage,

I<sub>OUT(max)</sub> is the maximum output current, for the application

IQ is the maximum quiescent current at IOUT(max).

A heat sink effectively increases the surface area of the package to improve the flow of heat away from the IC and into the surrounding air.

Each material in the heat flow path between the IC and the outside environment has a thermal resistance. Like series electrical resistances, these resistances are summed to determine  $R_{\Theta JA}$ , the total thermal resistance between the junction and the surrounding air.

- 1. Thermal Resistance of the junction to case,  $R_{\Theta JC}$  (°C/W)
- 2. Thermal Resistance of the case to Heat Sink,  $R_{\Theta CS}$  (°C/W)
- 3. Thermal Resistance of the Heat Sink to the ambient air,  $R_{\Theta SA}$  (°C/W)

These are connected by the equation:

$$R_{\Theta,JA} = R_{\Theta,JC} + R_{\Theta,CS} + R_{\Theta,SA}$$
 (3)

The value for  $R_{\Theta JA}$  is calculated using equation (3) and the result can be substituted in equation (1).

The value for  $R_{\Theta JC}$  is normally quoted as a single figure for a given package type based on average die size. For a high current regulator such as the CS5207-1 the majority of the heat is generated in the power transistor section. The value for  $R_{\Theta SA}$  depends on the heat sink type, while  $R_{\Theta CS}$ depends on factors such as package type, heat sink interface (is an insulator and thermal grease used?), and the contact area between the heat sink and the package. Once these calculations are complete, the maximum permissible value of  $R_{\Theta JA}$  can be calculated and the proper heat sink selected. For further discussion on heat sink selection, see application Management," document number "Thermal note AND8036/D, available through the Literature Distribution Center or via our website at http://onsemi.com.

#### **ADDITIONAL ORDERING INFORMATION**

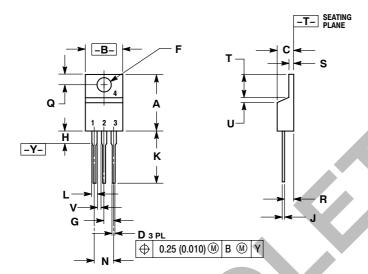
Orderable Part Number	Туре	Description	
CS5207-1GT3	7.0 A, Adj. Output	TO-220 THREE LEAD, STRAIGHT	



#### CS5207-1

#### PACKAGE DIMENSIONS

TO-220 **THREE LEAD T SUFFIX** CASE 221A-08 **ISSUE AA** 



#### NOTES:

- DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
- 2. CONTROLLING DIMENSION: INCH.

	INCHES		MILLIMETERS	
DIM	MIN	MAX	MIN	MAX
Α	0.560	0.625	14.23	15.87
В	0.380	0.420	9.66	10.66
С	0.140	0.190	3.56	4.82
D	0.025	0.035	0.64	0.89
F	0.139	0.155	3.53	3.93
G	0.100 BSC		2.54	BSC
Н		0.280		7.11
_	0.012	0.045	0.31	1.14
K	0.500	0.580	12.70	14.73
L	0.045	0.060	1.15	1.52
N	0.200	0.200 BSC		BSC
Q	0.100	0.135	2.54	3.42
R	0.080	0.115	2.04	2.92
S	0.020	0.055	0.51	1.39
Т	0.235 <	0.255	5.97	6.47
U	0.000	0.050	0.00	1.27
V	0.045		1.15	

#### PACKAGE THERMAL DATA

Paran	neter	TO-220 THREE LEAD	Unit
R <sub>OJC</sub>	Typical	1.6	°C/W
$R_{\Theta JA}$	Typical	50	°C/W

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